

Power System Analysis I **** Final *** 20.01.2012

Student name:

Number:

SOLUTIONS

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P1 (40): A 150 km, 230 kV, 60 Hz three-phase line has a positive-sequence series impedance $\bar{z} = 0.08 + j0.48 \Omega/\text{km}$ and a positive-sequence shunt admittance $\bar{y} = j3.33 \times 10^{-6} \text{ S/km}$. At full load, the line delivers 250 MW at 0.99 power factor lagging and at 220 kV. Using the nominal π circuit, calculate:

- the ABCD parameters,
- the sending-end voltage, current, and the real power,
- the percent voltage regulation, and (is this value acceptable?)
- the transmission-line efficiency at full load.
- Is the percent voltage regulation found in part c within the limit?

$$\bar{Z} = 12 + j72 = 73 \angle 80.54^\circ \Omega$$

$$\bar{Y} = j4.995 \times 10^{-4} = 5 \times 10^{-4} \angle 90^\circ \text{ S}$$

$$a) \quad \bar{A} = \bar{D} = \left[1 + \frac{(73 \angle 80.54^\circ)(5 \times 10^{-4} \angle 90^\circ)}{2} \right]$$

$$= \left[1 + \frac{-0.036 + j6 \times 10^{-3}}{2} \right] = 0.982 + j3 \times 10^{-3}$$

$$\bar{A} = \bar{D} = 0.982 \angle 0.175^\circ \text{ per-unit} \quad (6)$$

$$\bar{B} = \bar{Z} = 73 \angle 80.54^\circ \Omega \quad (2)$$

$$\bar{C} = 5 \times 10^{-4} \angle 90^\circ \left[1 + \frac{-0.036 + j6 \times 10^{-3}}{4} \right] = -7.5 \times 10^{-7} + j5 \times 10^{-4}$$

$$\bar{C} \approx 5 \times 10^{-4} \angle 90.1^\circ \text{ S} \quad (3)$$

$$b) \quad \bar{V}_S = \bar{A} \bar{V}_R + \bar{B} \bar{I}_R$$

$$\bar{V}_R = \frac{220}{\sqrt{3}} = 127 \text{ kV}_{LN}$$

$$\bar{I}_R = \frac{250 \times 10^6}{\sqrt{3}(220000)(0.99)} \angle -\cos^{-1}(0.99)$$

$$\bar{I}_R = 662.7 \angle -8.1^\circ \text{ A}$$

$$\bar{V}_S = (0.982 \angle 0.175^\circ)(127) + (73 \angle 80.54^\circ)(0.6627 \angle -8.1^\circ)$$

$$\bar{V}_S = 139.3 + j46.5 = 146.87 \angle 18.5^\circ \text{ kV}_{LN} \quad (7)$$

$$\bar{I}_S = (5 \times 10^{-4} \angle 90.1^\circ)(127) + (0.982 \angle 0.175^\circ)(0.6627 \angle -8.1^\circ)$$

$$\bar{I}_S = 0.6444 - j0.02622 = 0.645 \angle -2.33^\circ$$

$$\bar{I}_S = 645 \angle -2.33^\circ \text{ A} \quad (7)$$

P2 (35): A three-phase, 60 Hz, completely transposed 765 kV, and 400 km uncompensated transmission line has the following positive-sequence line constants:

$$\bar{z} = 0.02 + j0.4 \text{ } \Omega/\text{km}$$

$$\bar{y} = j6 \times 10^{-6} \text{ S/km}$$

The sending-end voltage is held constant at the rated line voltage. Assuming a lossless line, determine the following:

- The theoretical steady-state stability limit in MW and in terms of SIL.
- The practical line loadability in MW and in terms of SIL.
- The full-load current at 0.92 lagging power factor based on the above practical line loadability.

$$a) \quad P_{Rmax} = \frac{V_S \cdot V_R}{X'}$$

$$Z_C = \sqrt{\frac{j0.4}{j6 \times 10^{-6}}} = 258.2 \text{ } \Omega$$

$$\bar{\gamma} = j\beta = \sqrt{j0.4(j6 \times 10^{-6})} = 1.5492 \times 10^{-3}$$

$$X' = 258.2 \sin(0.62)$$

$$\beta l = 0.62 \text{ RAD}$$

$$X' = 150 \text{ } \Omega$$

$$P_{Rmax} = \frac{(765 \times 10^3)(765 \times 10^3)}{150} = \underline{\underline{3902 \text{ MW}}} \quad (10)$$

$$SIL = \frac{765^2}{258.2} = 2267 \text{ MW} \quad (2)$$

$$\underline{P_{Rmax} = 1.72 SIL} \quad (4)$$

$$b) \quad P_R = \frac{765 \times (0.95 \times 765) \sin(35^\circ)}{150} = \underline{\underline{2126 \text{ MW}}} \quad (10)$$

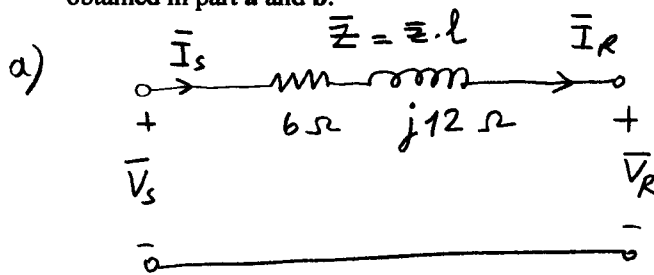
$$\underline{P_R = 0.9377 SIL} \quad (2)$$

$$c) \quad \bar{I}_R = \frac{2126 \times 10^6}{\sqrt{3} (0.95 \times 765000) (0.92)} \angle -\cos^{-1}(0.92)$$

$$\underline{\bar{I}_R = 1836 \angle -23.07^\circ} \text{ A} \quad (7)$$

P3(25) A 60 km, 69 kV, 60 Hz three-phase line has positive-sequence series impedance $\bar{z} = 0.1 + j0.2 \Omega/\text{km}$. The load at the receiving-end draws a current of 500 Ampere. Assume that the sending-end voltage is held constant at the rated line voltage.

- Calculate the magnitude of the receiving-end voltage if the load power factor is 0.866 lagging
- Calculate the magnitude of the receiving-end voltage if the load power factor is 0.6 leading
- Comment about the effect of the load power factor on the voltage regulation of the line based on the results obtained in part a and b.



$$\bar{V}_R = 39837 - (6 + j12) 500 \angle -30^\circ$$

$$\bar{V}_R = 34438 \angle -6.16^\circ \text{ V}$$

$$V_R = 34438 \text{ V}$$

b)

$$\bar{V}_R = 39837 - (6 + j12) 500 \angle 53.13^\circ$$

$$\bar{V}_R = 43255 \angle -7.97^\circ \text{ V}$$

$$V_R = 43255$$

(8)

(8)

c) for the result in part a: $\frac{34438}{39837} = 0.865$

this result is less than 0.95 . poor regulation

This is due to lagging power factor.

(9)

For the result in part b: $\frac{43255}{39837} = 1.086 \text{ pu}$

Not acceptable since it is more than 1.05 pu .

The high voltage is due the leading power factor.

The ABCD parameters of a medium line

$$\bar{A} = \bar{D} = \left(1 + \frac{\bar{z} \cdot \bar{y}}{2}\right) \text{ per-unit}$$

$$\bar{B} = \bar{Z} \Omega$$

$$\bar{C} = \bar{Y} \cdot \left(1 + \frac{\bar{z} \cdot \bar{y}}{2}\right) \text{ S}$$

The exact ABCD parameters of a lossless line

$$\bar{A} = \bar{D} = \cos \beta l \text{ per-unit}$$

$$\bar{B} = jZ_c \sin \beta l \Omega$$

$$\bar{C} = j \frac{1}{Z_c} \sin \beta l \text{ S}$$

Real power delivered by a lossless line is

$$P_R = \frac{V_S V_R}{X'} \sin \delta \text{ W}$$

$$X' = Z_c \sin \beta l \Omega$$

$$\bar{Z}_c = \sqrt{\bar{z} / \bar{y}} \Omega$$

$$\bar{y} = \sqrt{\bar{z} \cdot \bar{y}} \text{ m}^{-1}$$

Real power delivered by a lossless line in terms of SIL is

$$P_R = V_{Spu} V_{Rpu} (\text{SIL}) \frac{\sin \delta}{\sin(\beta l)}$$